

# MODELING OF THE AFTER-EFFECTS OF OXYGENATED INFLOWS IN ANOXIC FJORDS SYSTEMS

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Germany

# Anoxic conditions in the water column

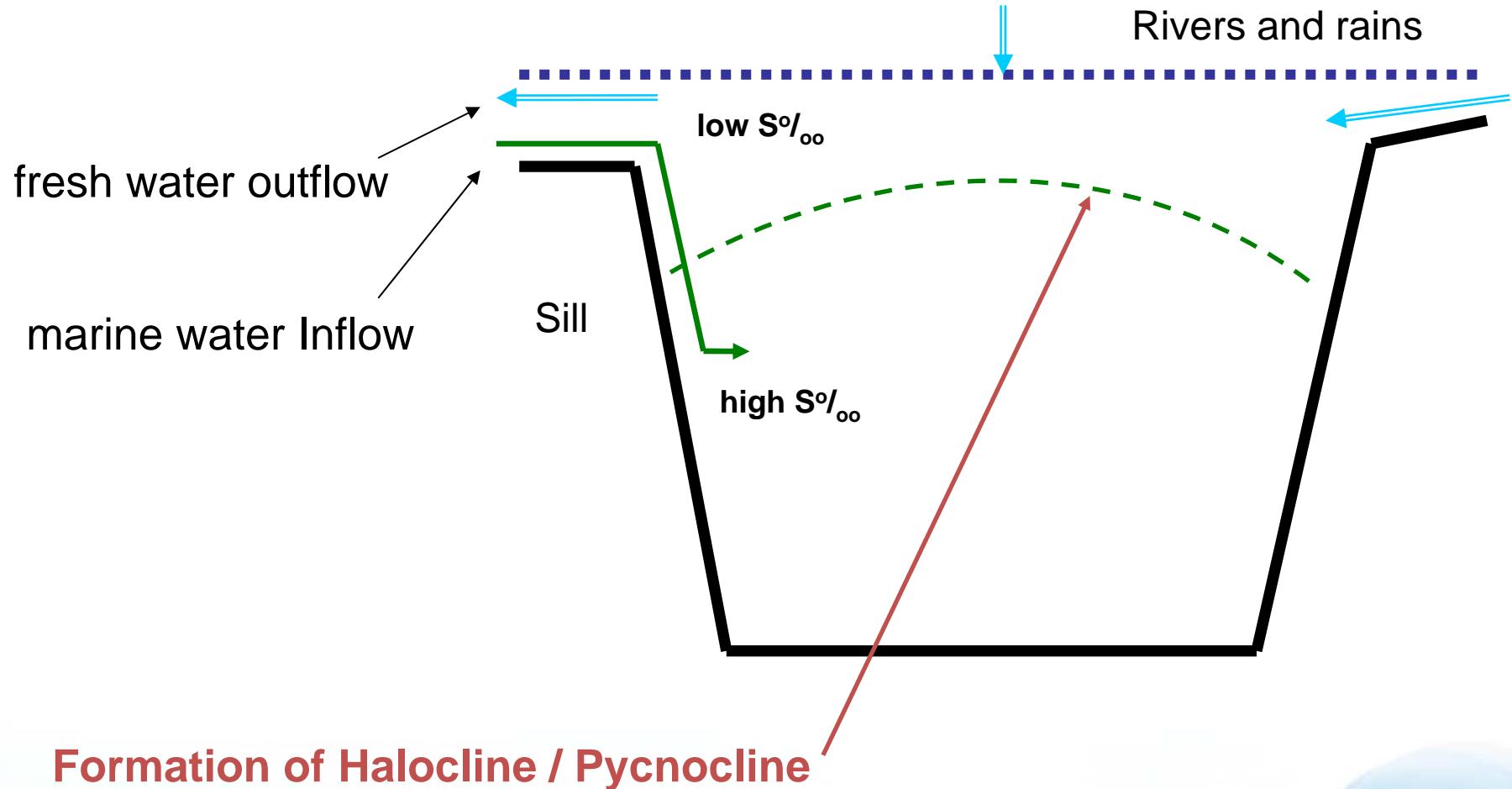
**Common feature in numerous areas in coastal and marginal seas**

**Affected by natural and anthropogenic factors:**

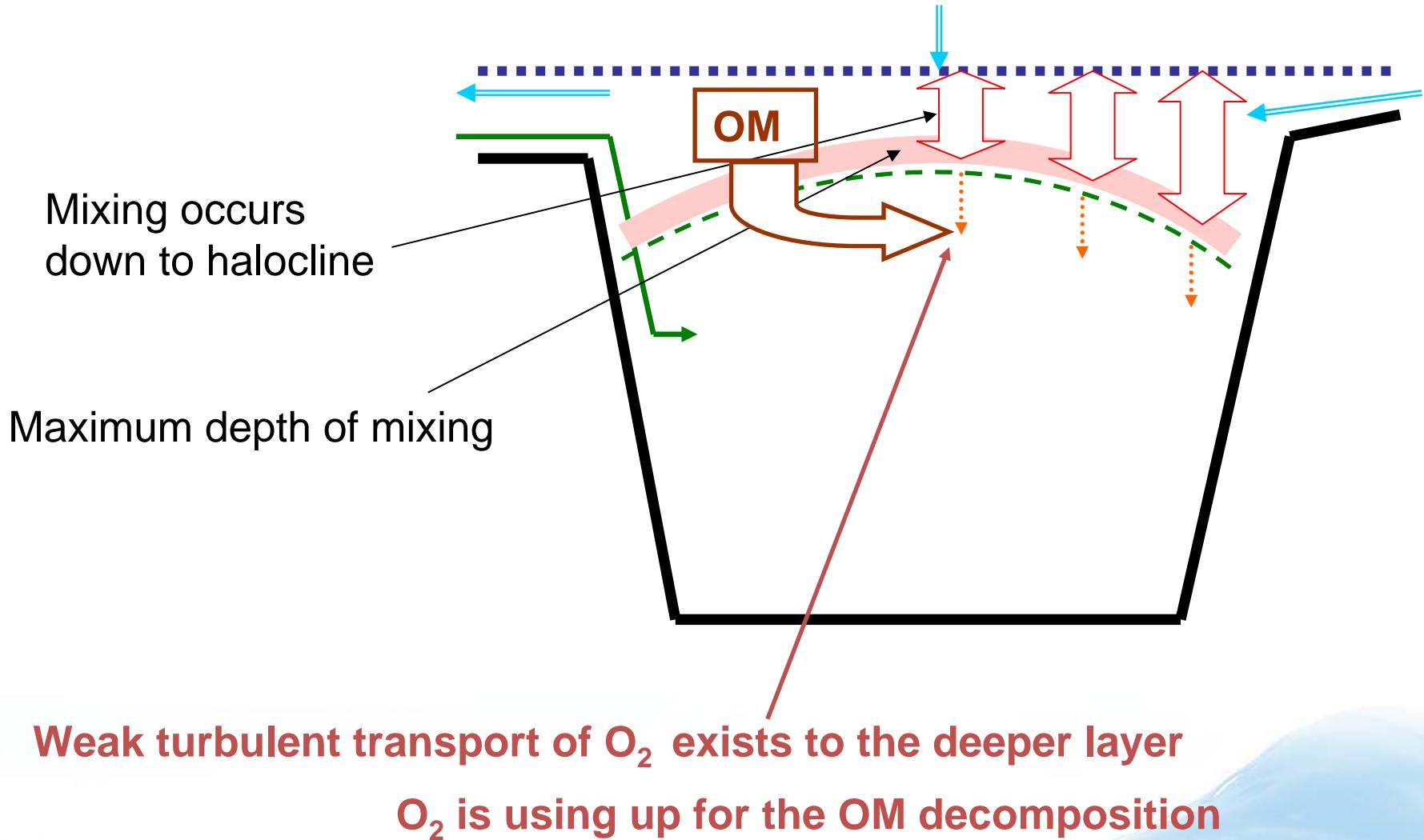
- intensity of aeration
- amount of produced OM

**The appearance of water anoxia is a threat for the functioning of healthy coastal ecosystems and thereby a direct danger to human health and economic welfare of coastal societies.**

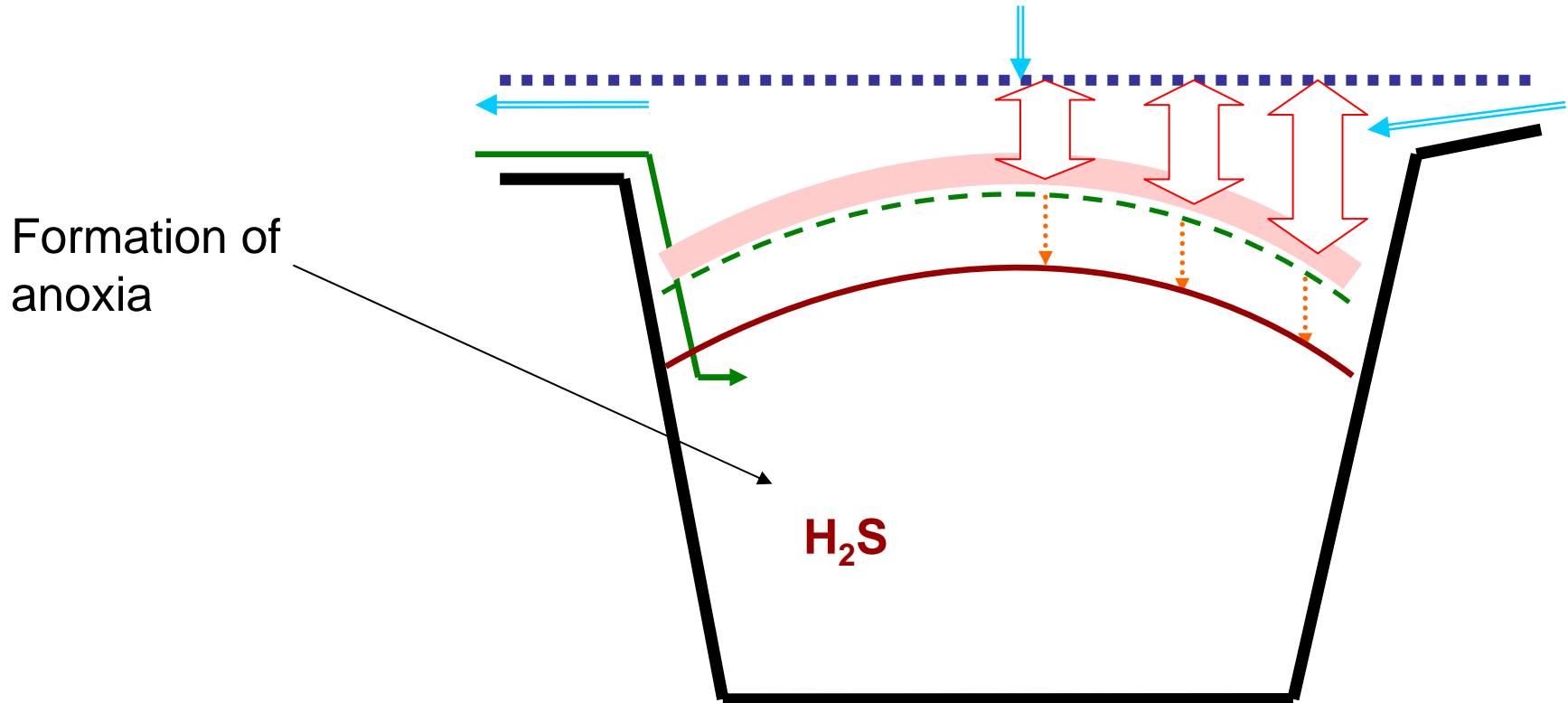
# Anoxic conditions in the water column



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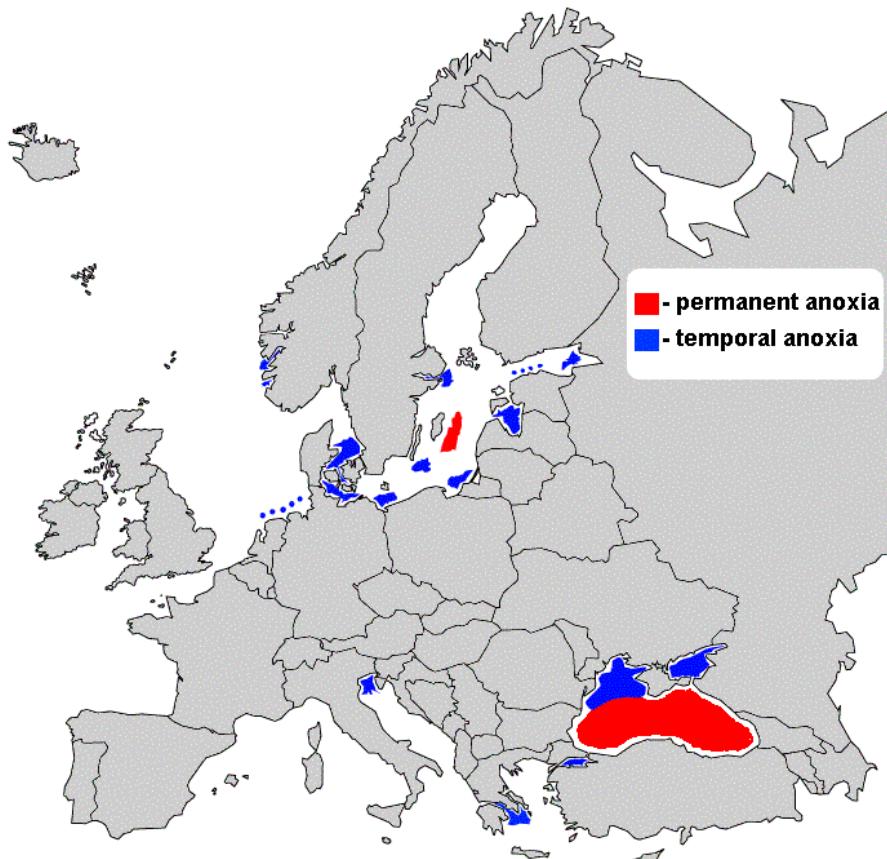


# Anoxic conditions in the water column



Flux of OM is not balanced by the flux of O<sub>2</sub>  
and OM is decomposed with other electron-acceptors.

# Anoxic conditions in the water column

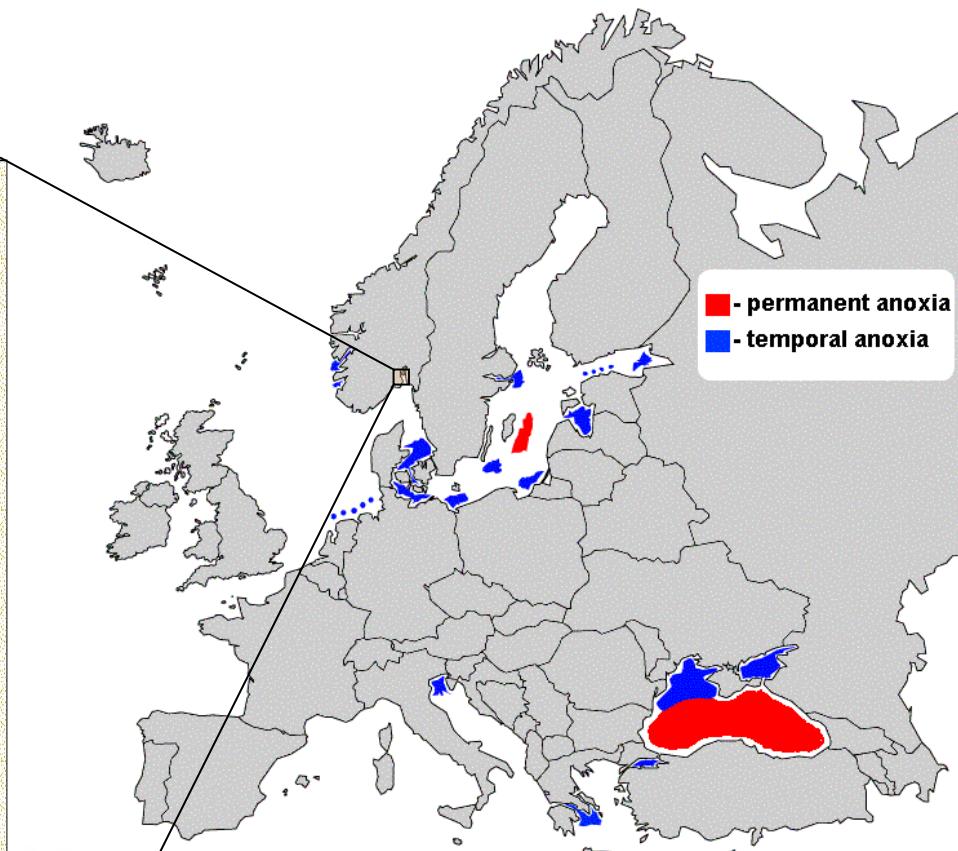
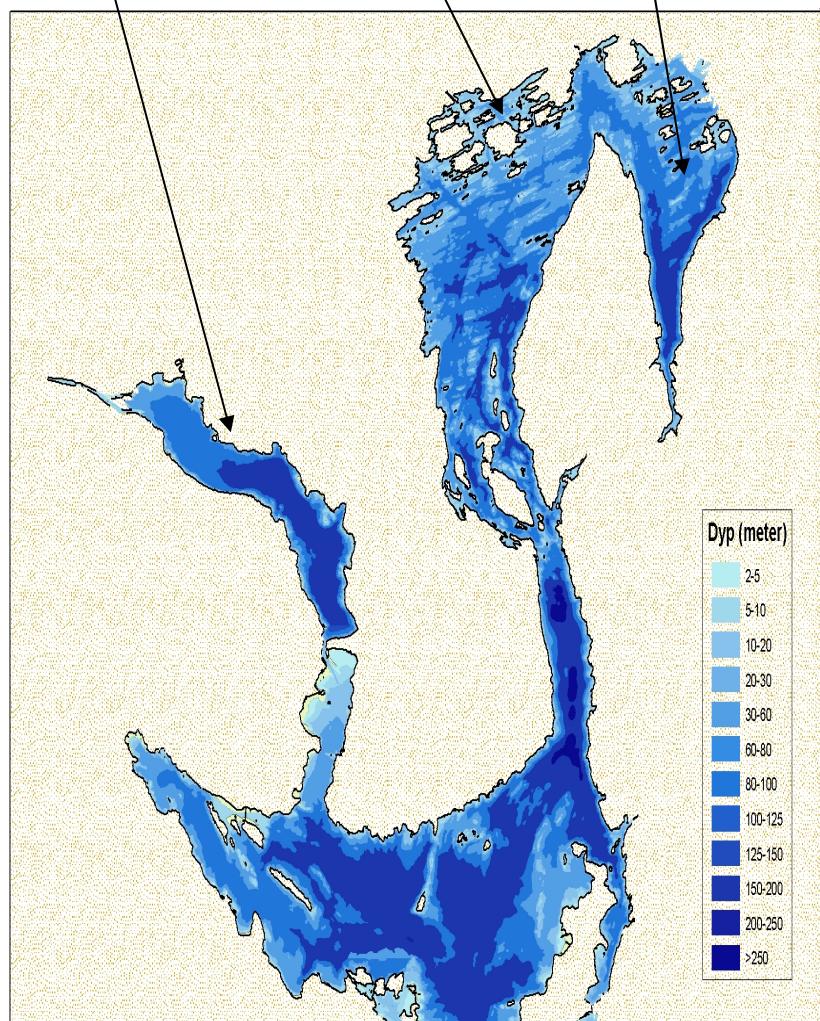


# Anoxic conditions in the water column

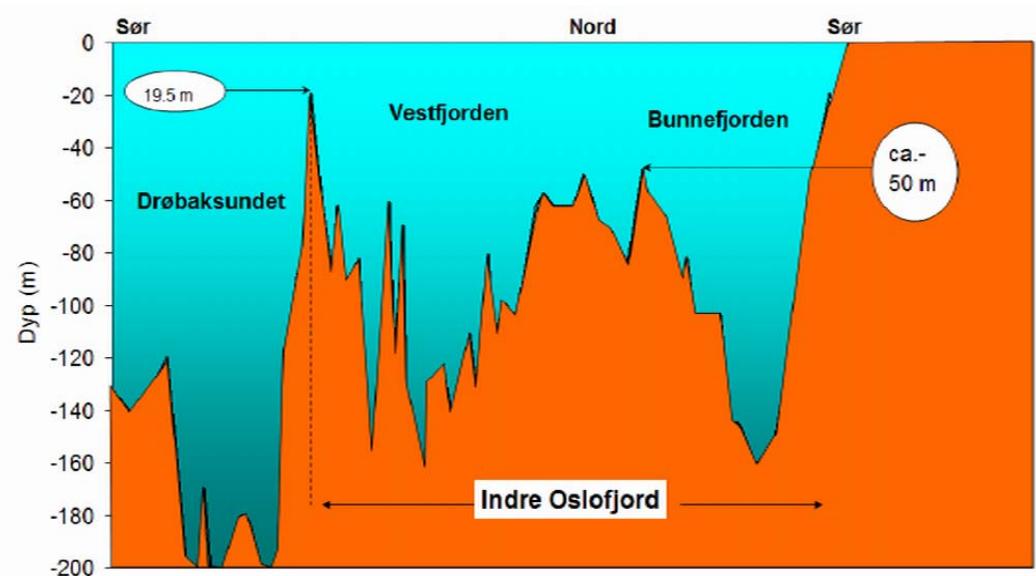
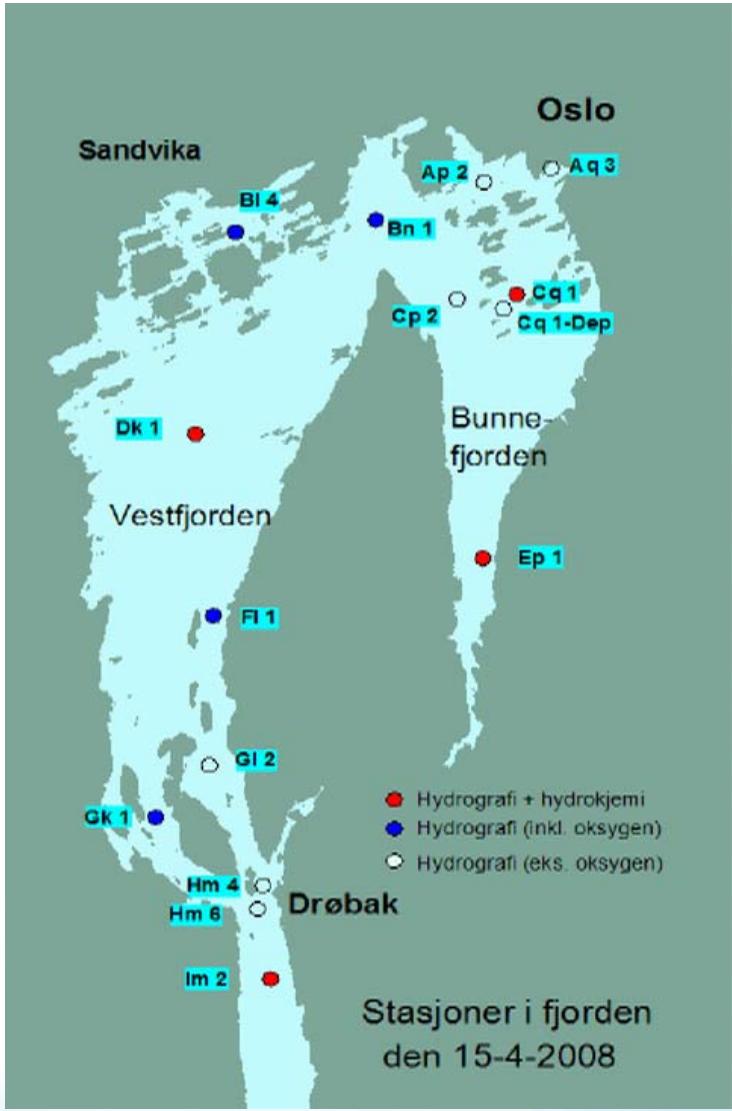
Drammensfjord  
(Richards, 1965)

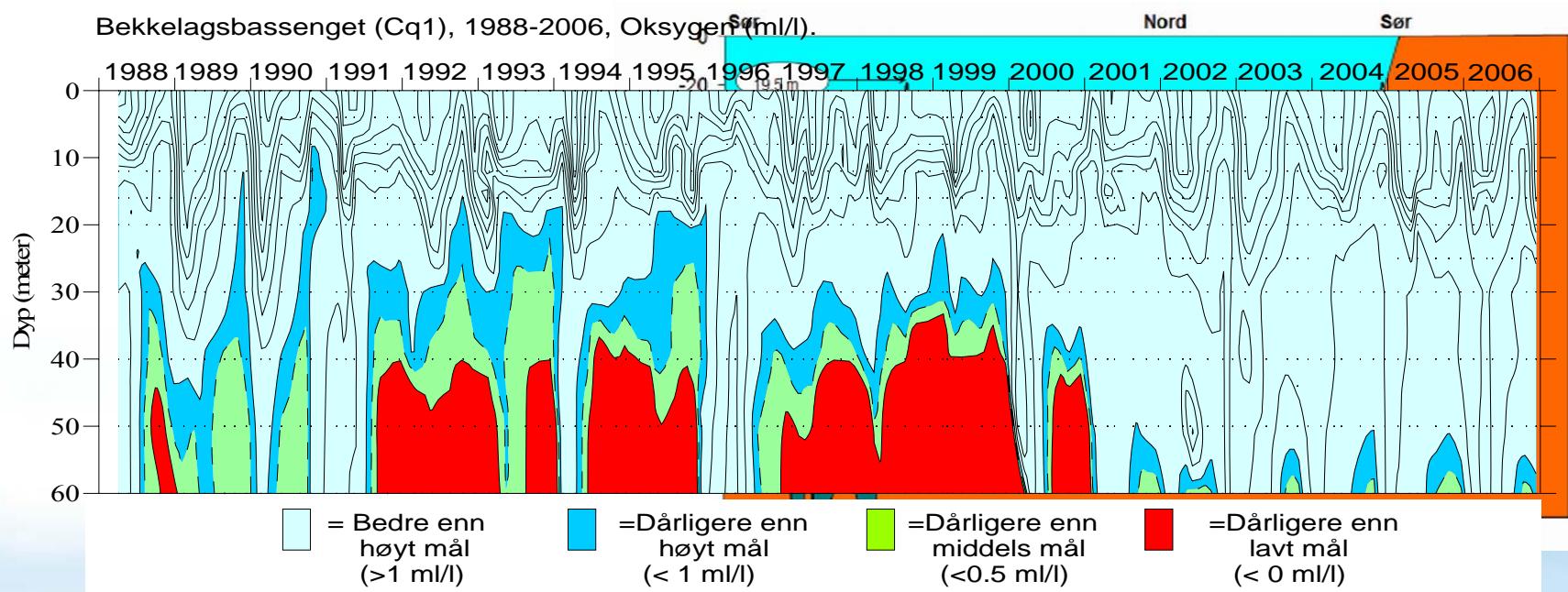
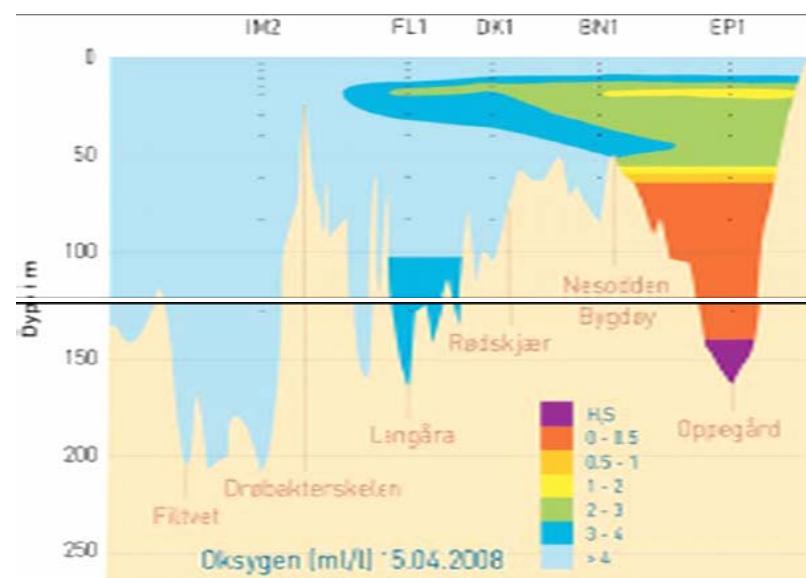
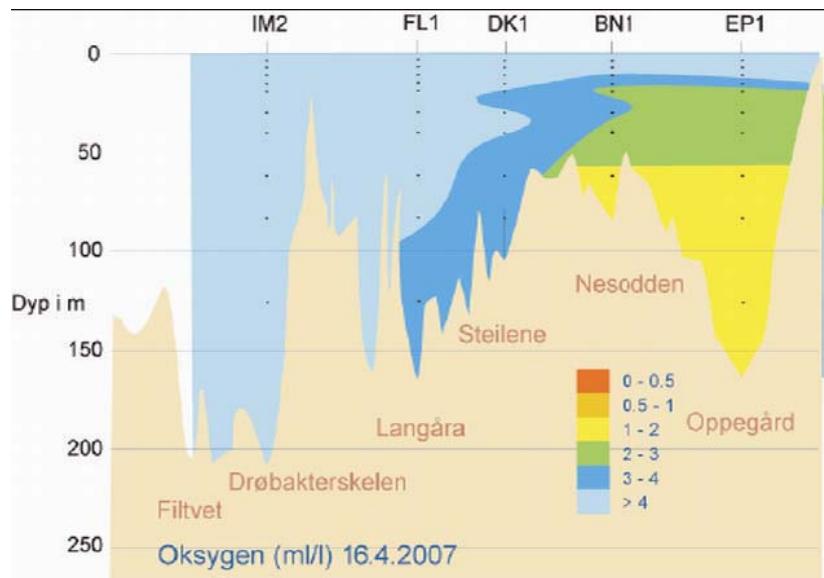
Baerumsbassenget

Bunnefjord



# Oslofjord



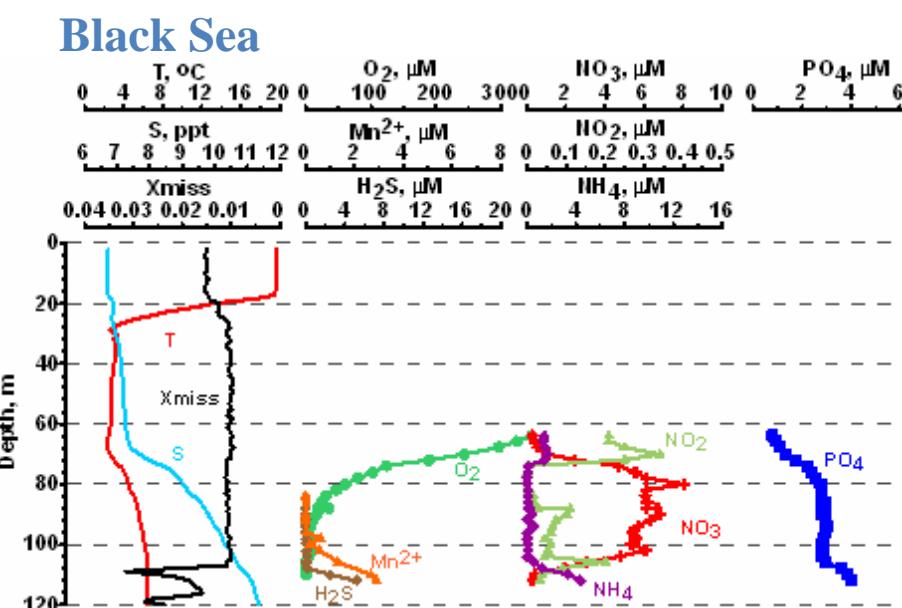
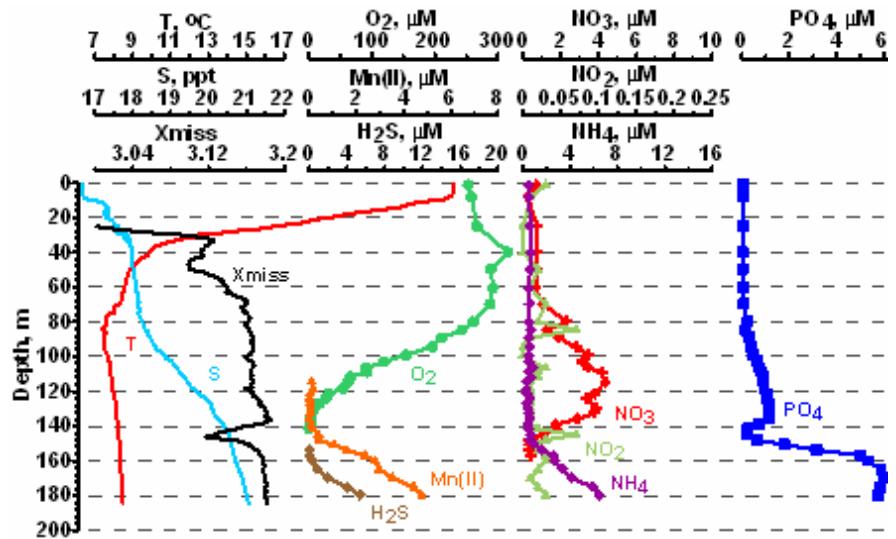
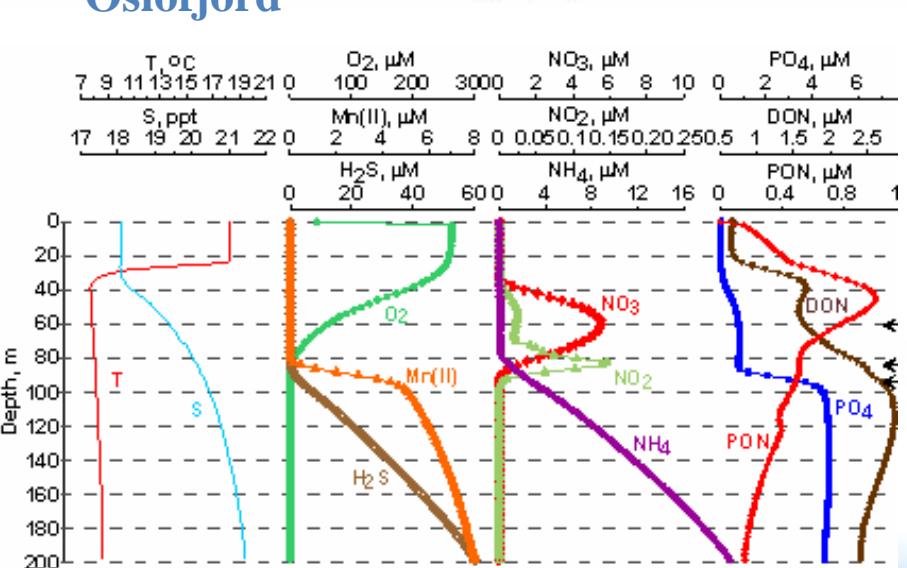
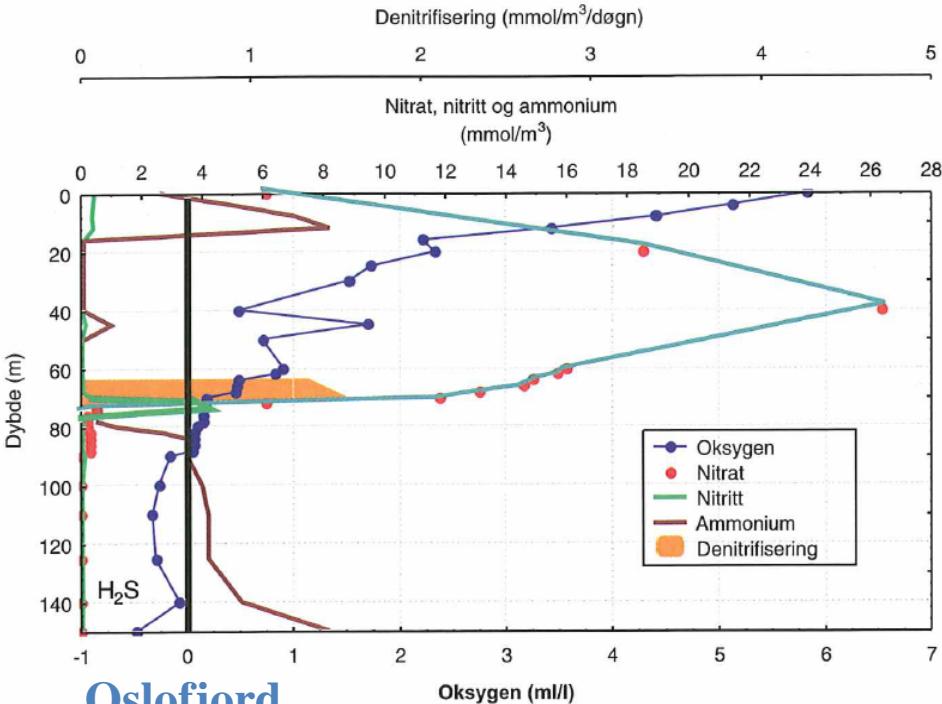


## Questions:

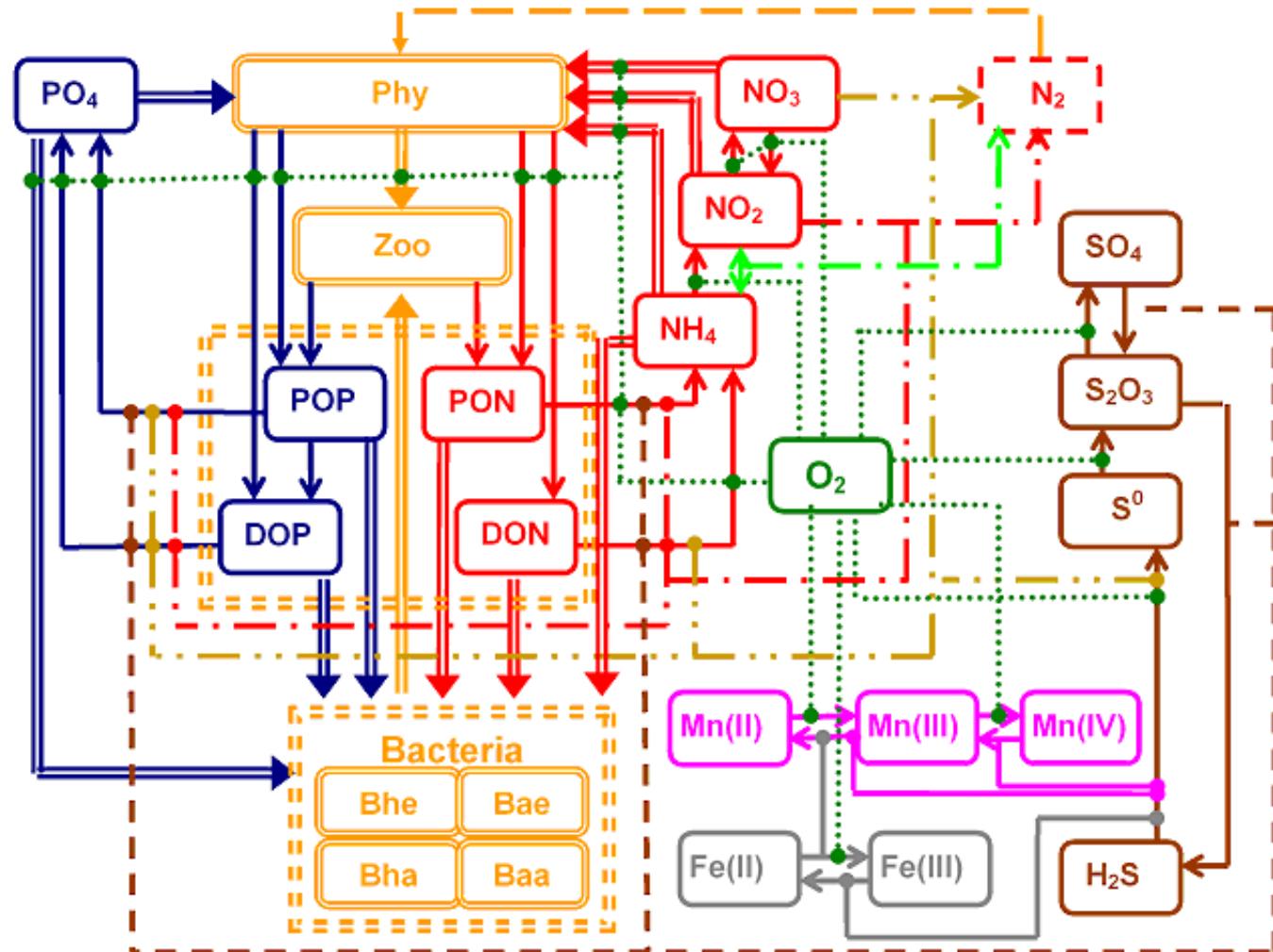
What happens during the periods of stagnation and flushing:

- Are the main processes at the redox interface in equilibrium?
- Is the redox interface characterized by the same chemical structure?

# Redox interface structure



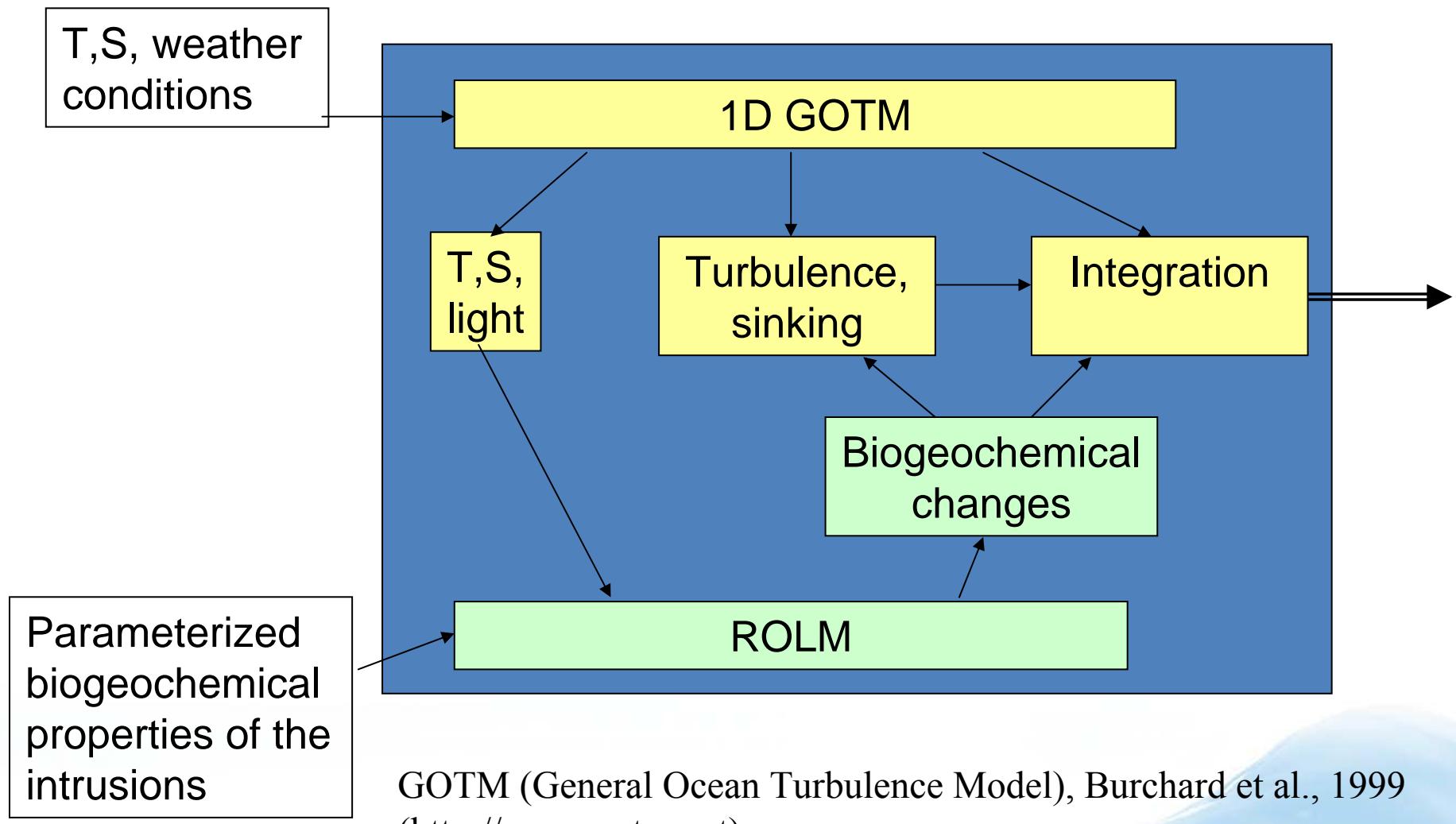
# ROLM biogeochemical model



ROLM (Redox Layer Model). Yakushev et al., 2007.

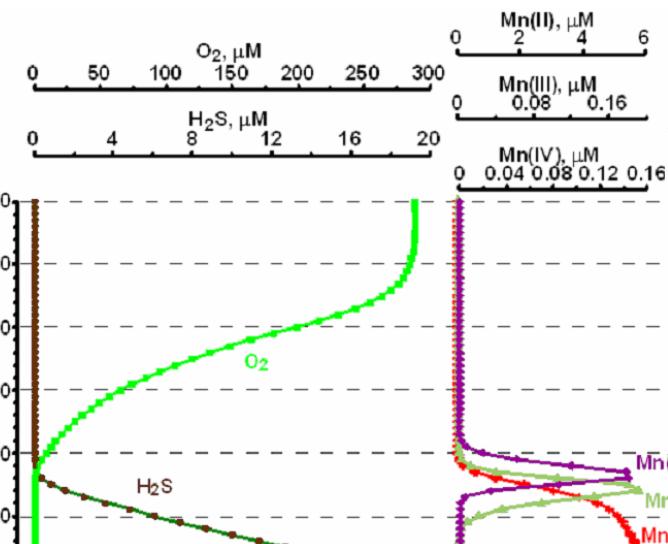
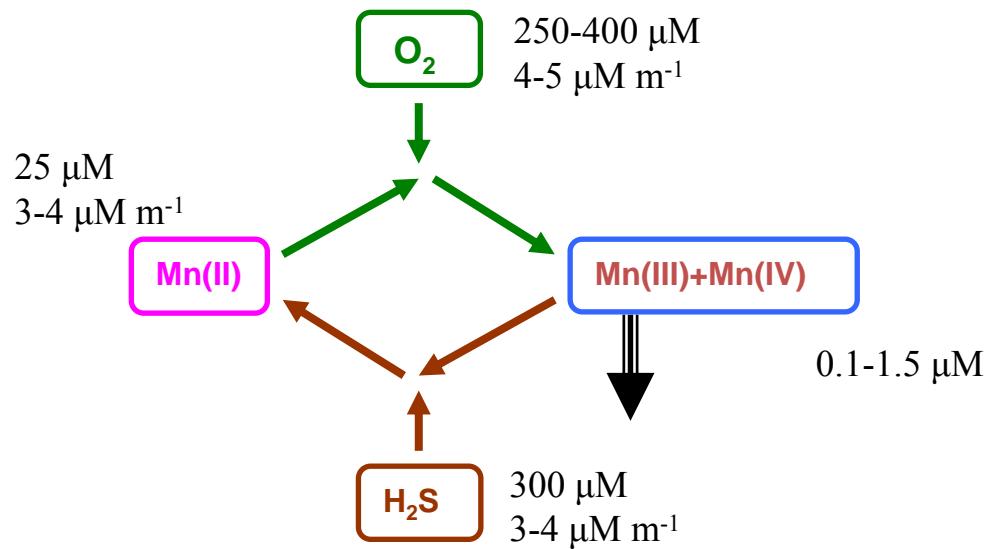
[http://www.io-warnemuende.de/documents/mebe68\\_2007-yakushev.pdf](http://www.io-warnemuende.de/documents/mebe68_2007-yakushev.pdf)

## Scheme of calculations:



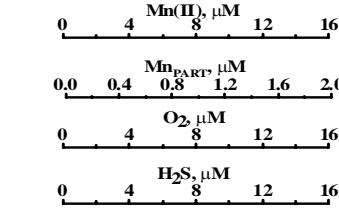
GOTM (General Ocean Turbulence Model), Burchard et al., 1999 (<http://www.gotm.net>).

# Vertically balanced structure:

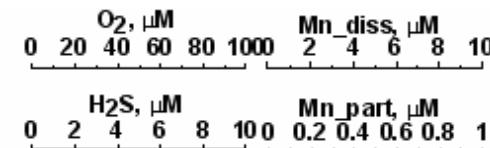
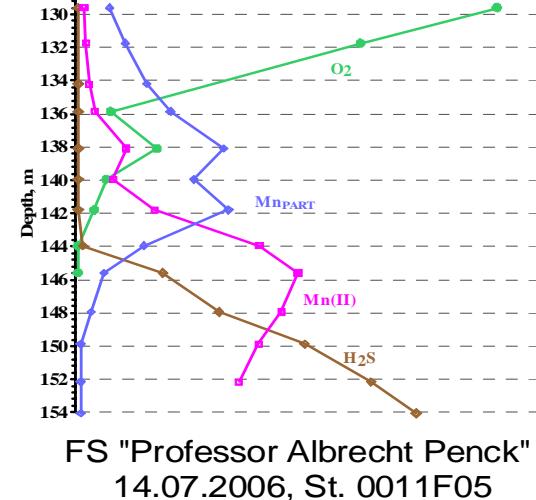


Model

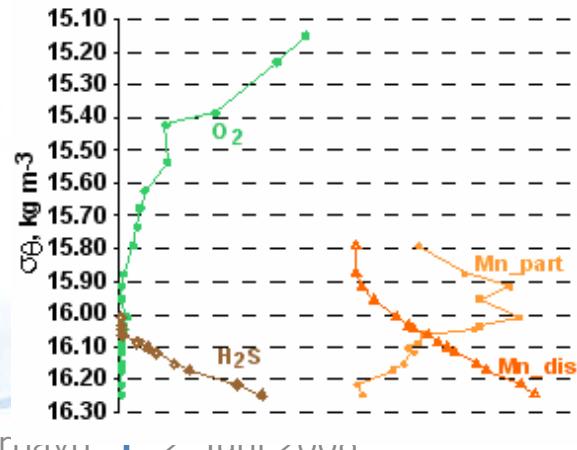
NIVA



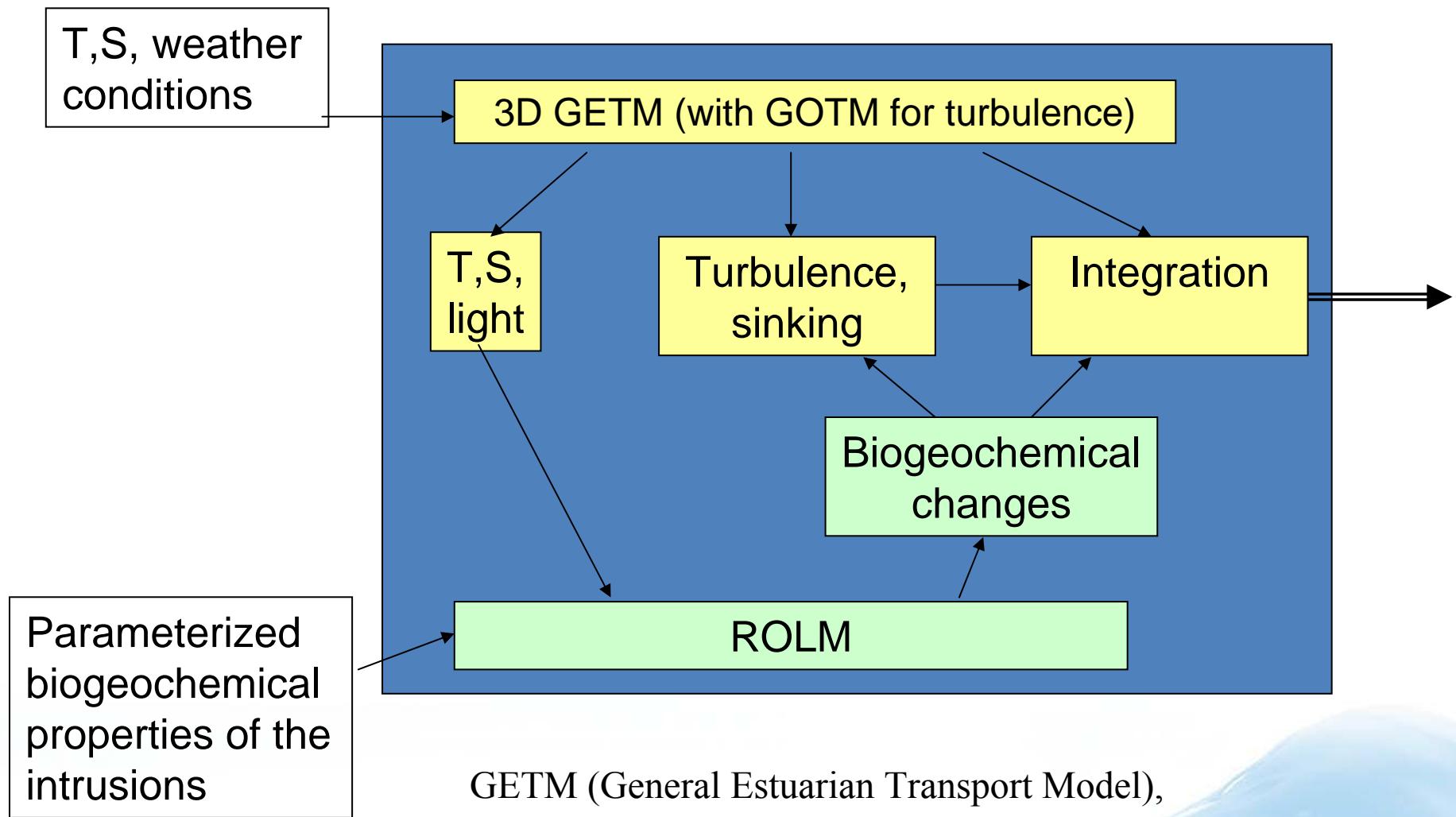
Gotland



Black Sea



# Scheme of calculations:

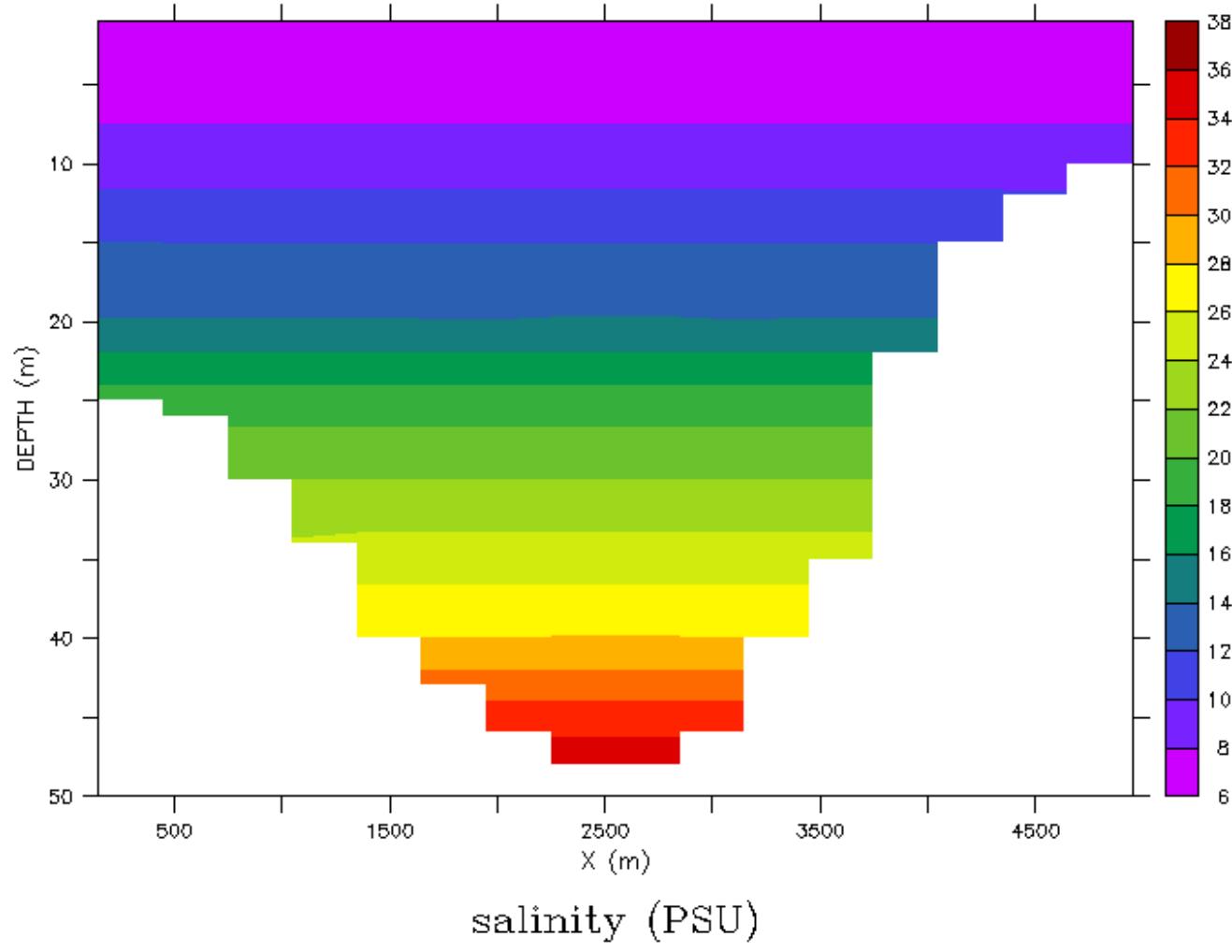


GETM (General Estuarian Transport Model),  
<http://www.bolding-burchard.com/html/GETM.htm>

Y (m) : 750  
TIME : 01-JAN-2003 00:00

DATA SET: fjord

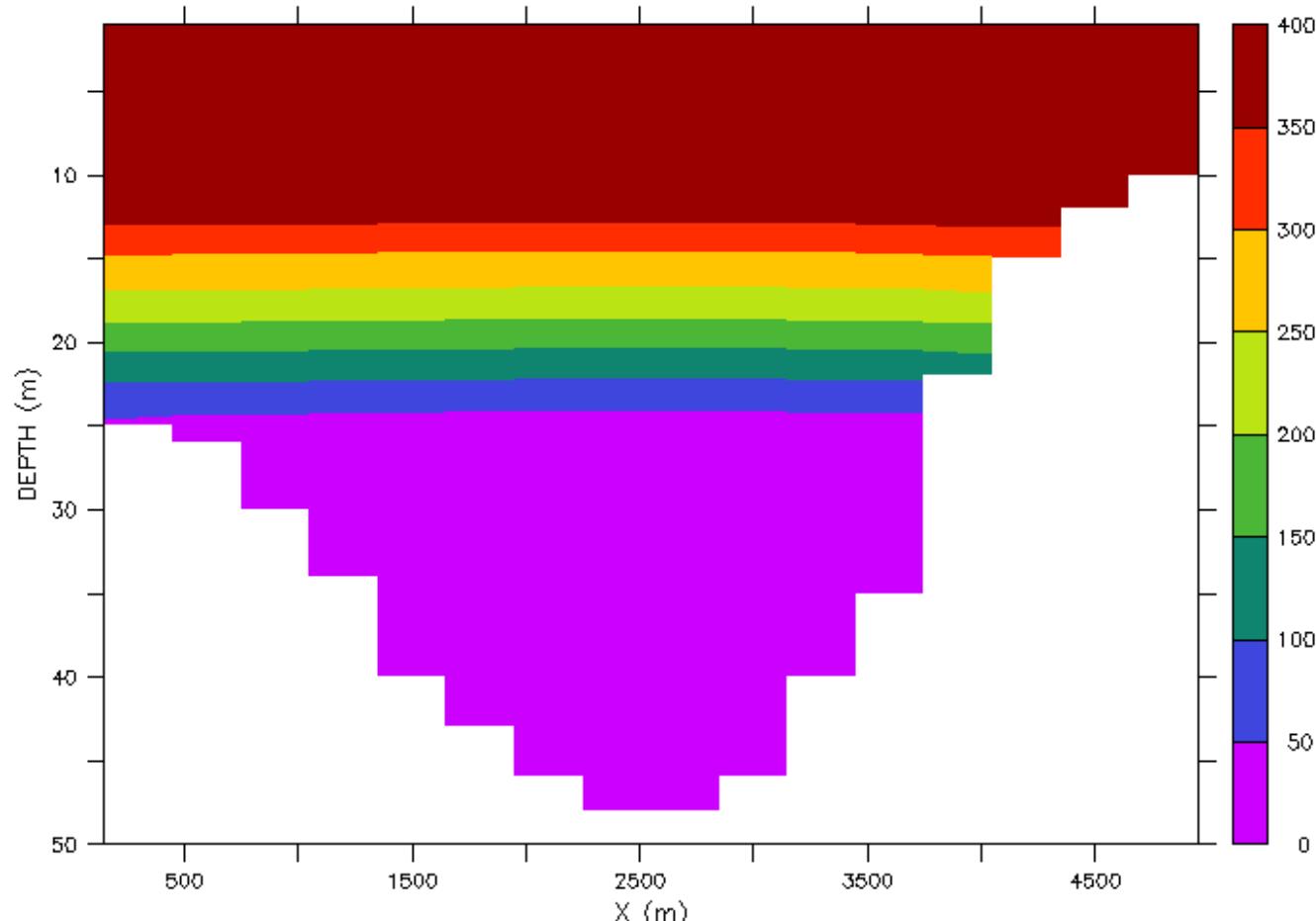
GETM-Output with zax



Y (m) : 750  
TIME : 01-JAN-2003 00:00

DATA SET: fjord

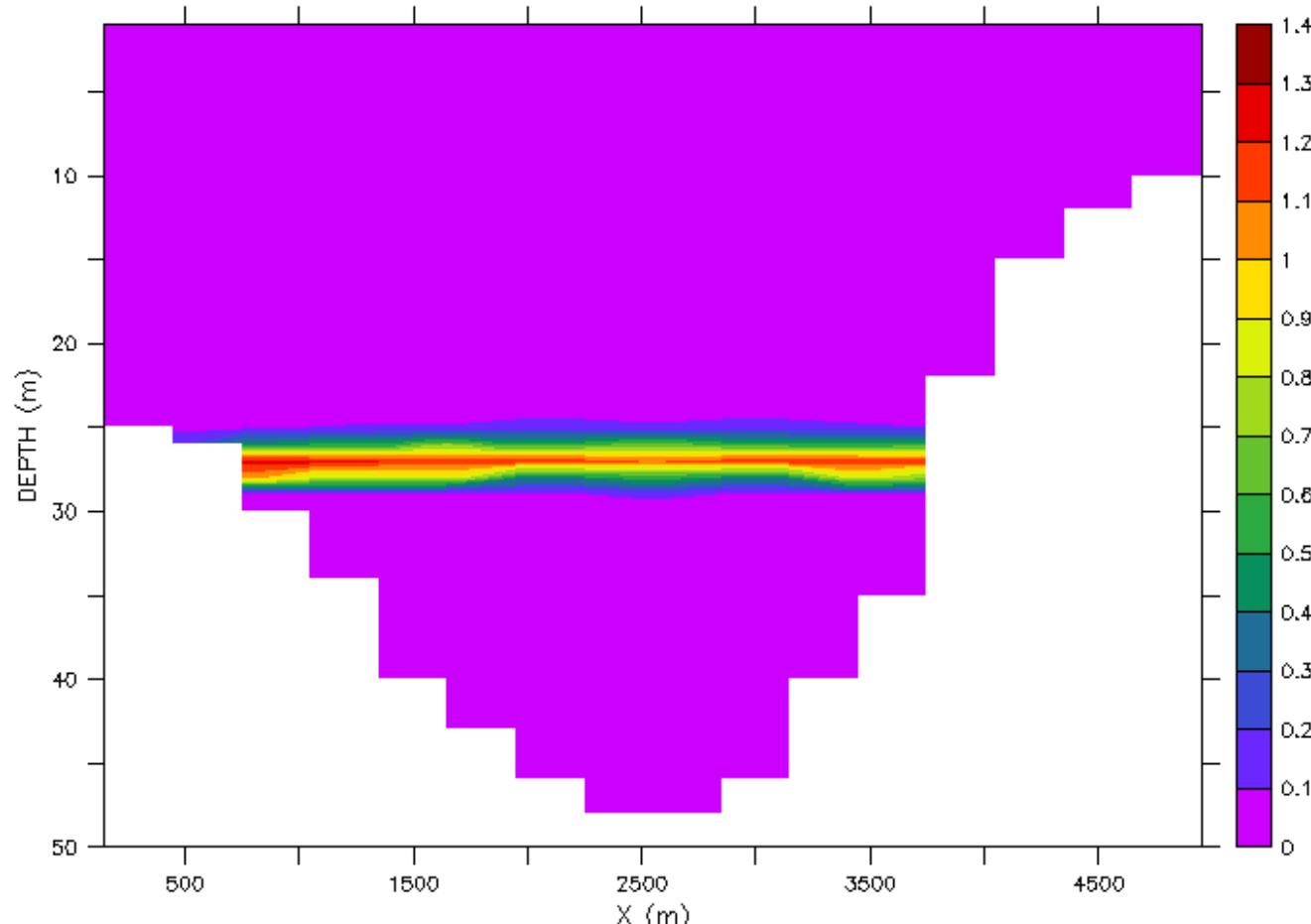
GETM-Output with zax



Y (m) : 750  
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DATA SET: fjord2

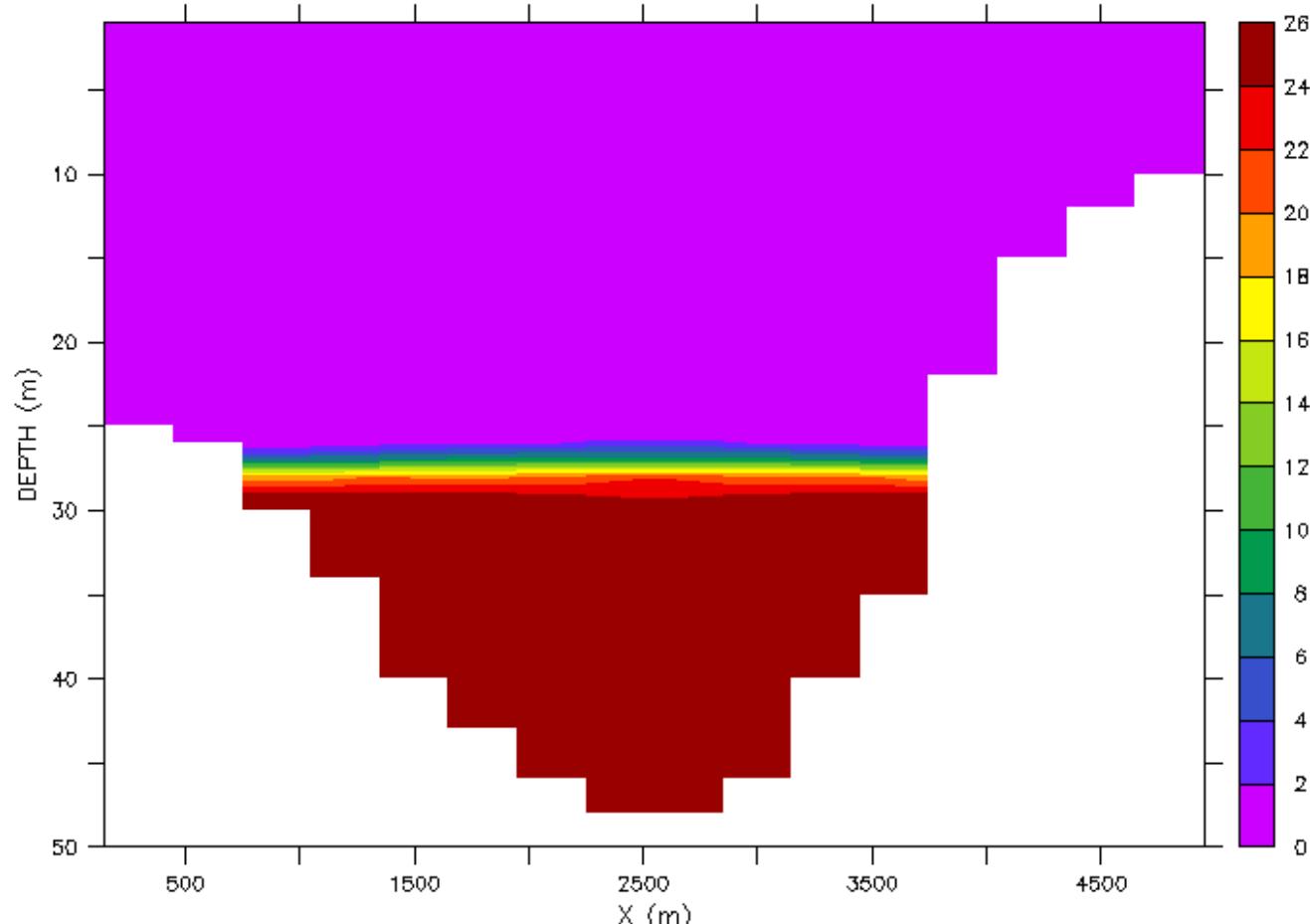
GETM-Output with zax



Y (m) : 750  
TIME : 01-JAN-2003 00:00

DATA SET: fjord2

GETM-Output with zax



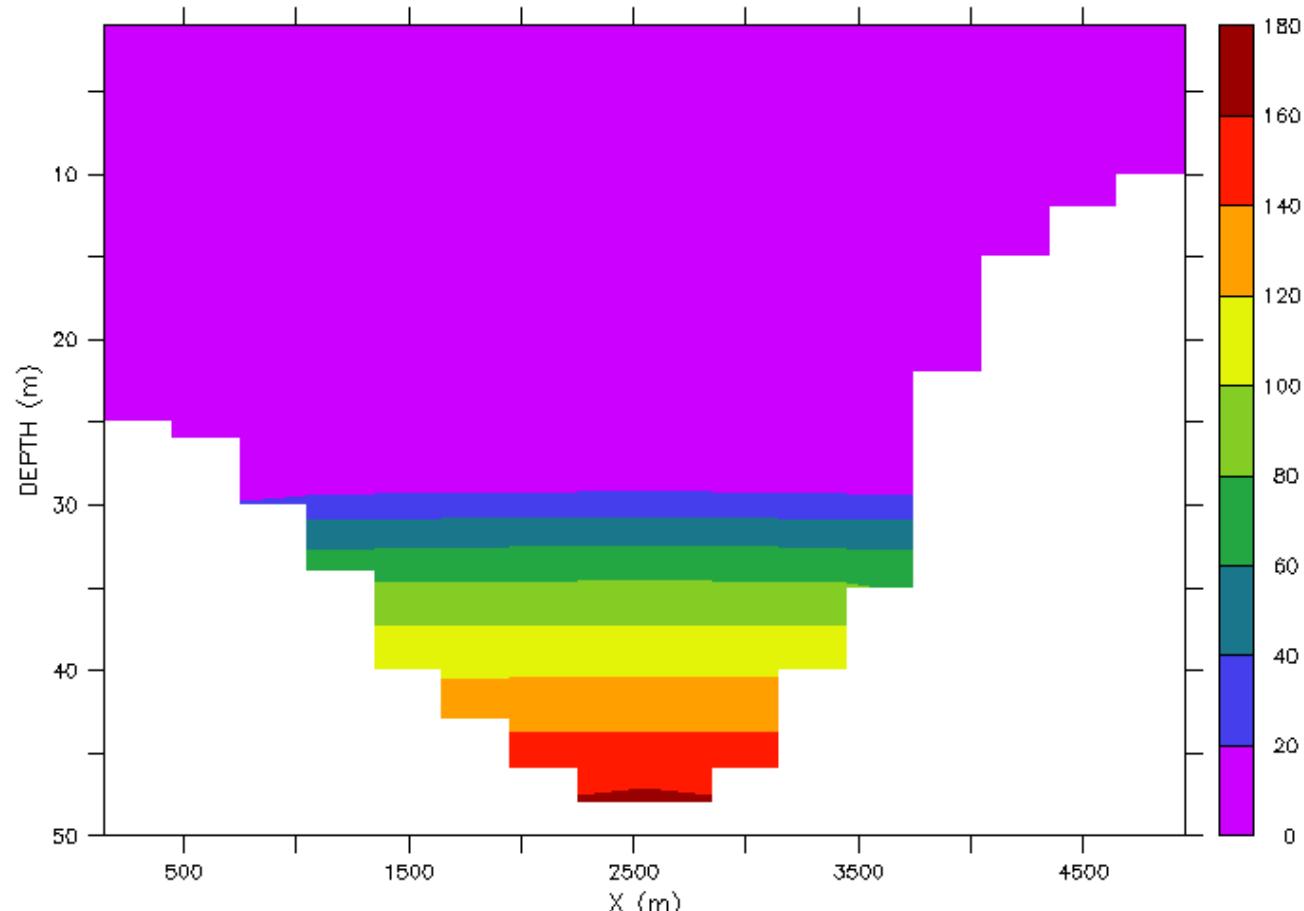
bivalent\_manganese (mmol mn/m<sup>3</sup>)

FERRET Ver. 6.02  
NOAA/PWEL THAP  
May 18 2008 16:26:48

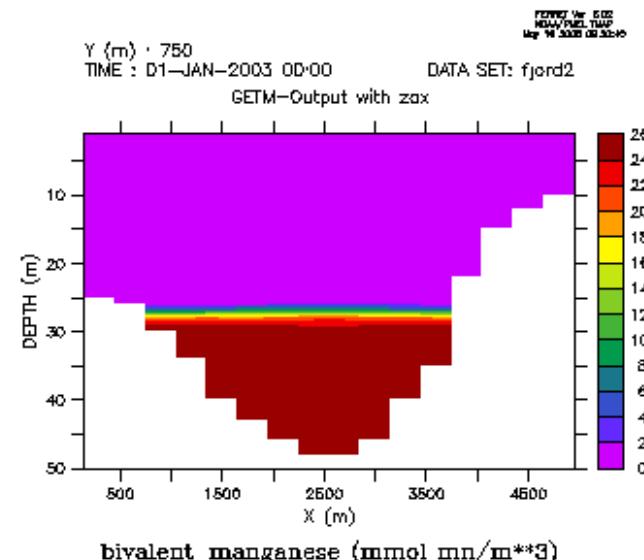
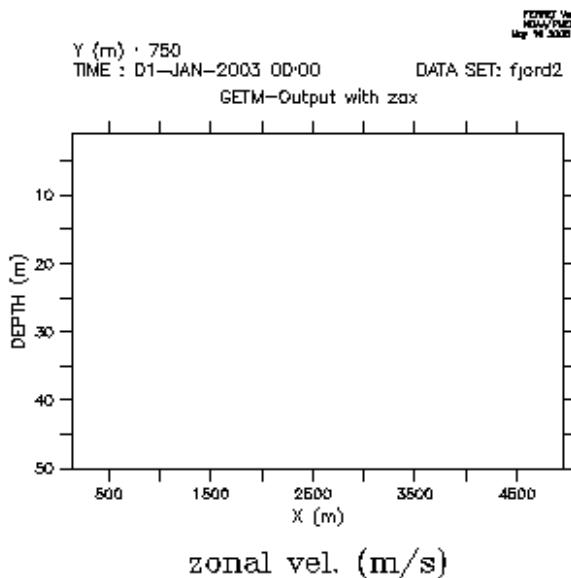
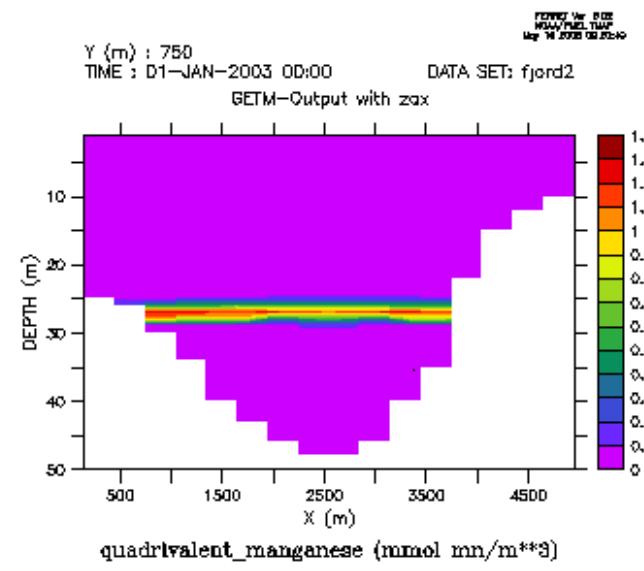
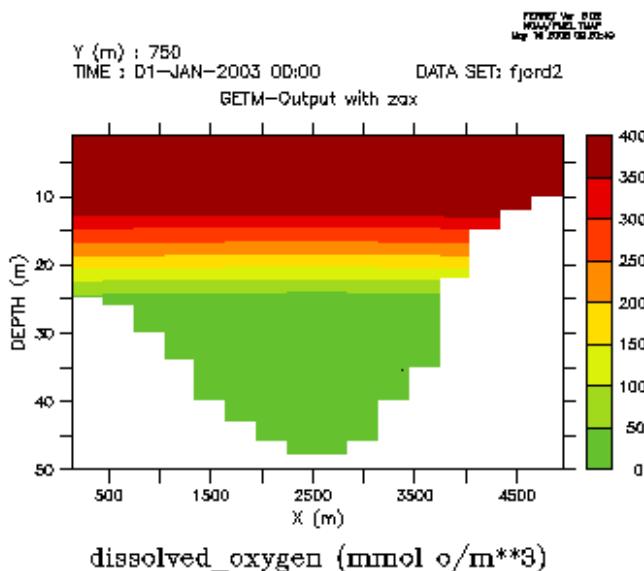
Y (m) : 750  
TIME : 01-JAN-2003 00:00

DATA SET: fjord2

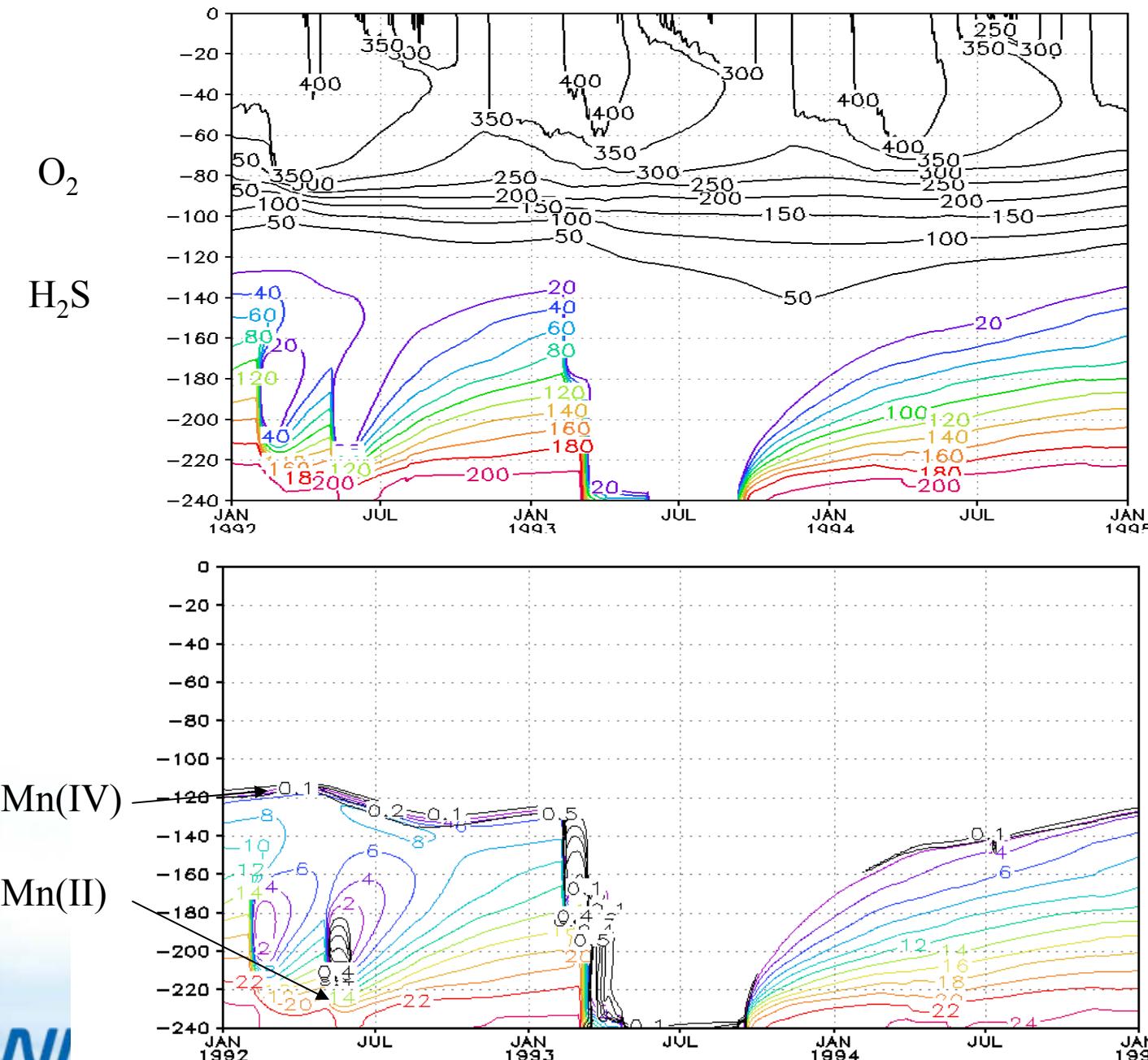
GETM-Output with zax

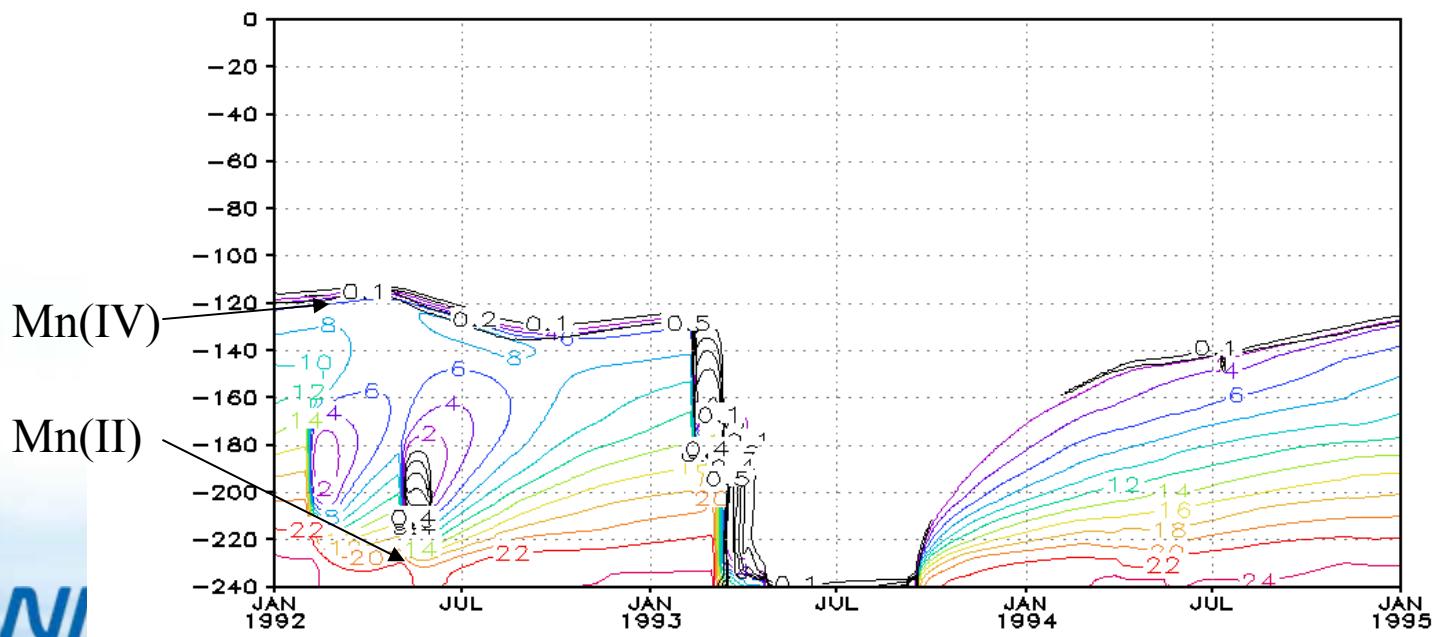
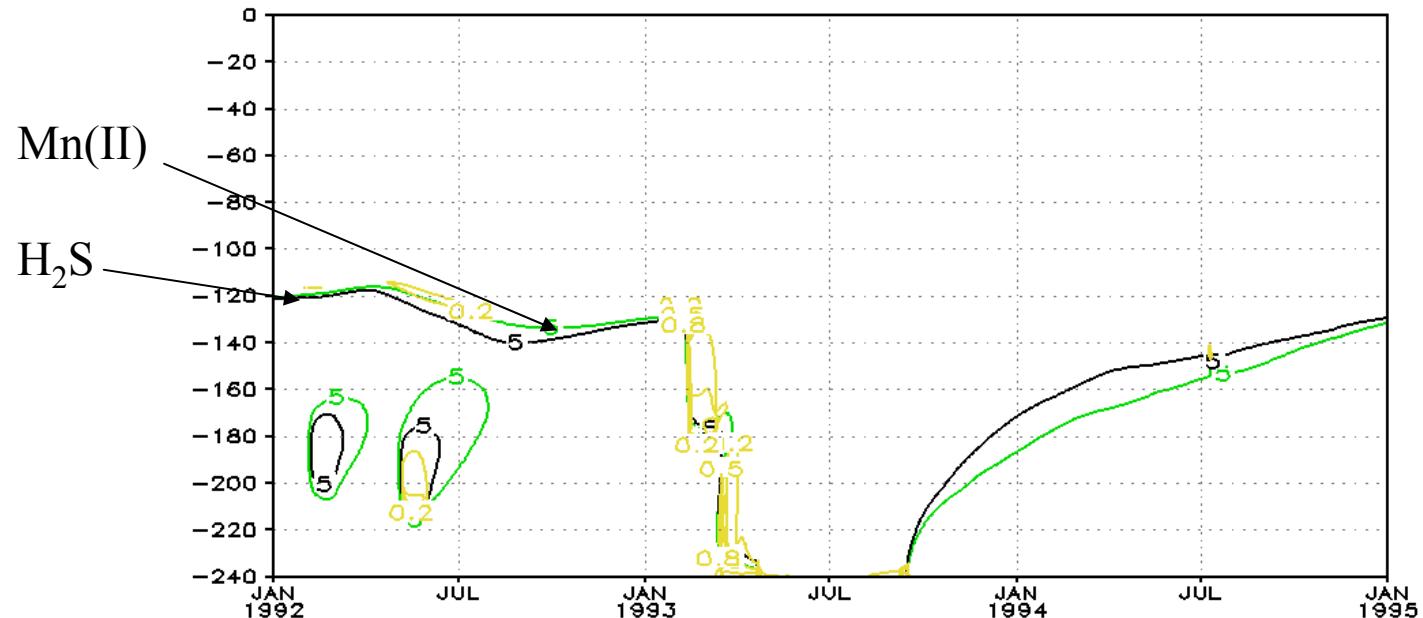


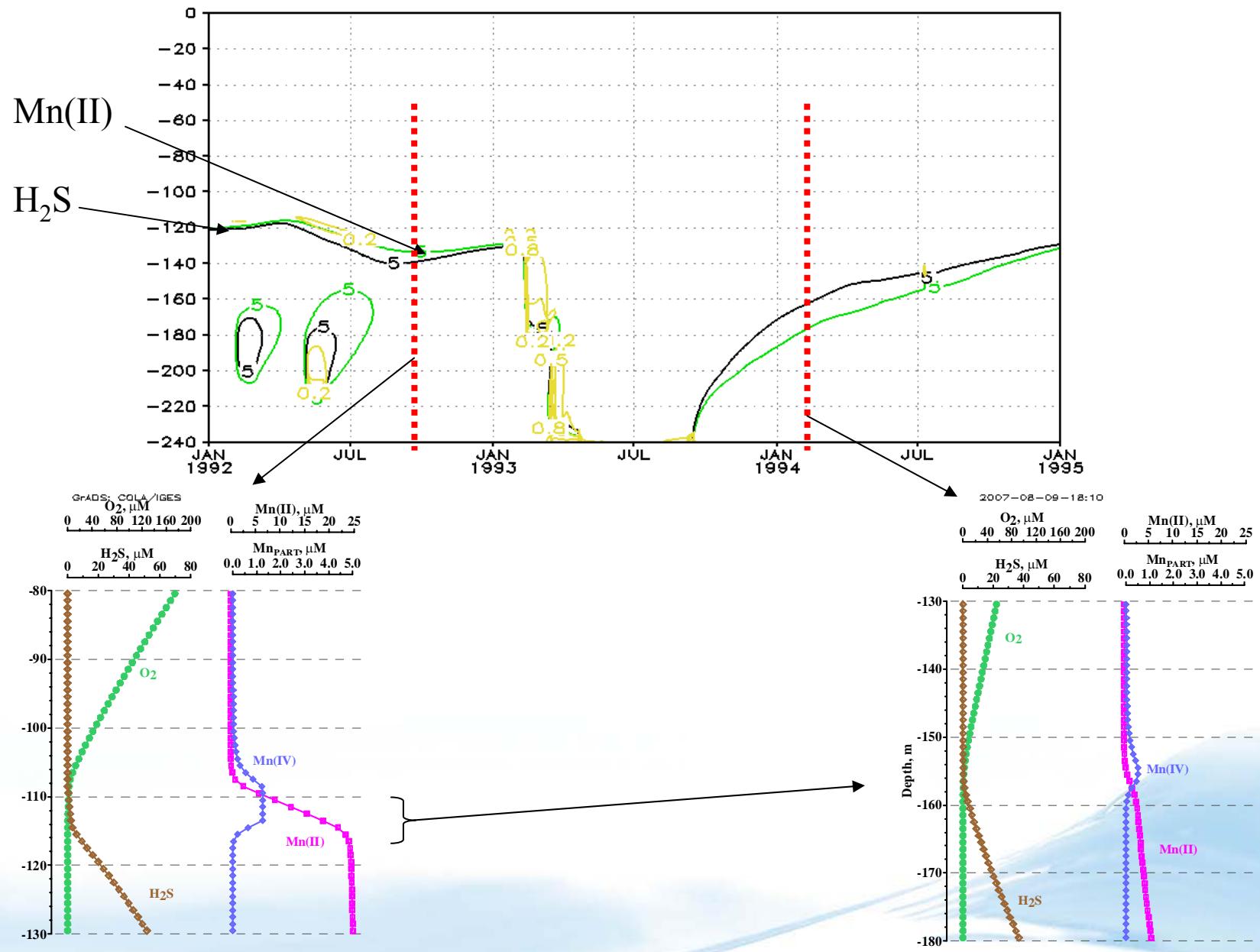
hydrogen\_sulfide (mmol s/m\*\*3)

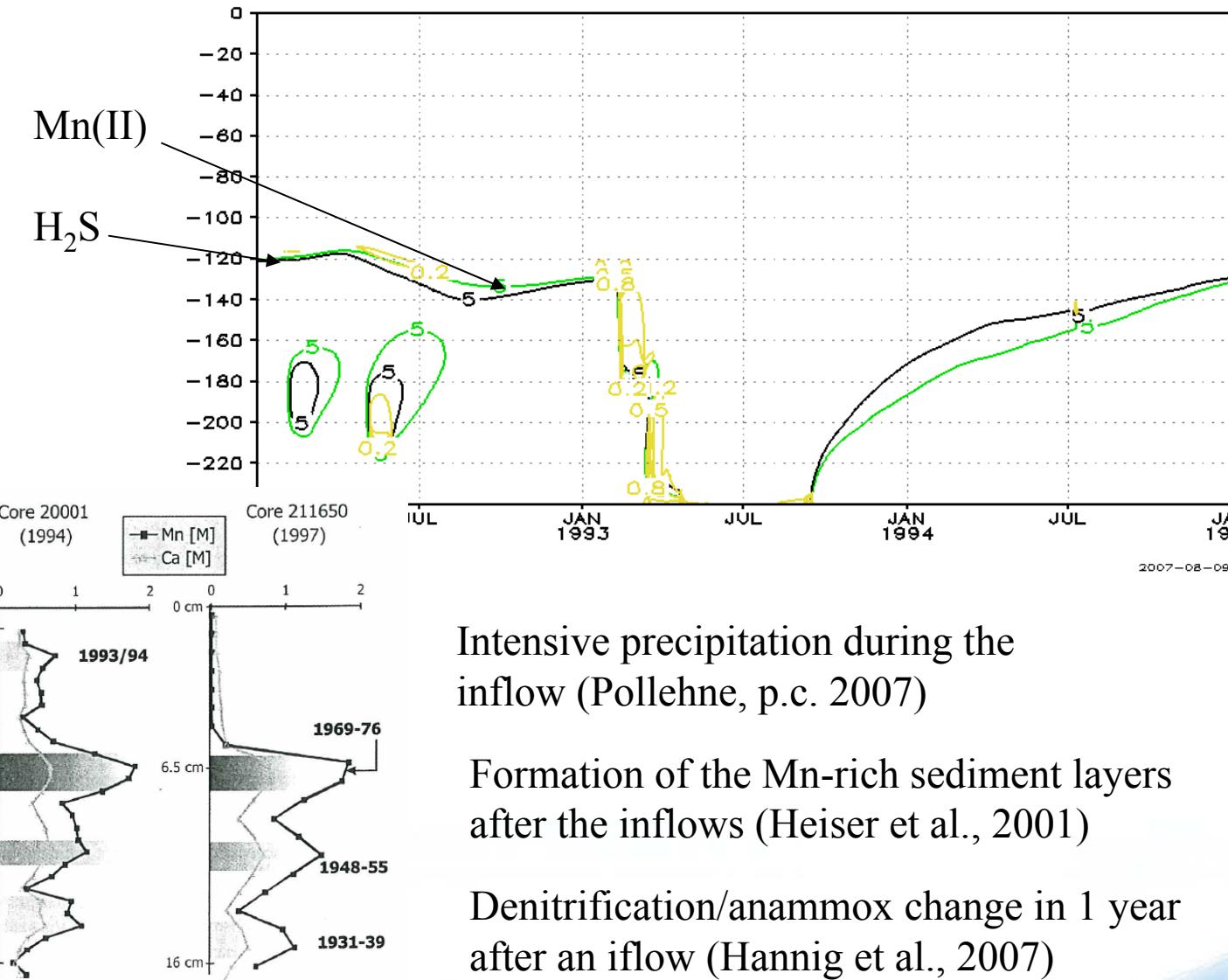


# 1D modeling of temporal variability:





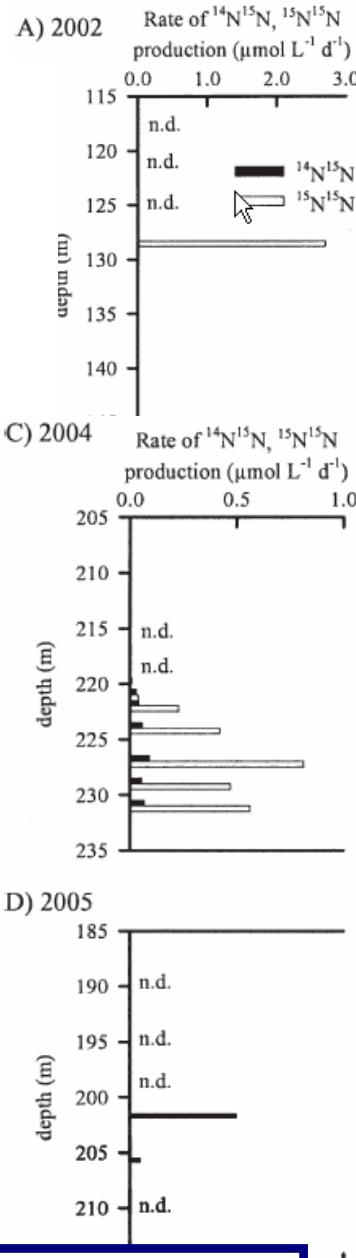




Intensive precipitation during the inflow (Pollehne, p.c. 2007)

Formation of the Mn-rich sediment layers after the inflows (Heiser et al., 2001)

Denitrification/anammox change in 1 year after an iflow (Hannig et al., 2007)



> 2 years required for the reestablishment of the stable redox interface structure...

Fig. 8. Solid phase profiles of core 211650 (July 1997) and 20001 (August 1994, Neumann et al., 1997).

# Conclusions

- Periods of oxygenated inflows are characterized by sudden increase of particulate Mn(IV) and vanishing of the total Mn from the water column.
- Periods of reestablishing of the anoxic conditions are characterized my inbalanced redox structure with absence of Mn(IV) maximum between O<sub>2</sub> and H<sub>2</sub>S.
- Application of the models (2D, 3D) can be usefull for analysing and prediction of the reactions of the oxygen-deficient and anoxic systems on the possible changes of climatic (mixing events) and anthropogenic factors (eutrophication).



# Thank you !

# Boundary conditions

## Upper boundary:

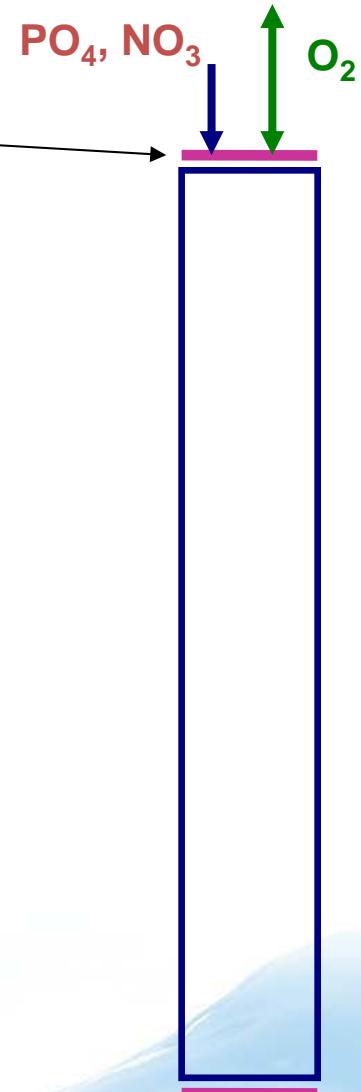
$\text{PO}_4, \text{NO}_3$ :  $Q_P^u = 0.0085 \text{ mmol m}^{-2} \text{ d}^{-1}$

$Q_{NO_3}^u = 0.46 \text{ mmol m}^{-2} \text{ d}^{-1}$  (HELCOM, 2002)

$O_2$ :  $Q_{O_2} = k_{660} (Sc/660)^{-0.5} (Oxsat - O_2)$   
 $k_{660} = 0.365 u^2 + 0.46 u$

*Oxsat* (T,S) is the  $O_2$  saturation concentration (UNESCO, 1986);  
*Sc* is the Schmidt number

$C_i$ :  $Q_{C_i}^u = 0.$



# Boundary conditions

## Lower boundary:

**Phy,Zoo,Bact,PON,POP:**  $Q_{C_i} = -(B_u w^{Sink} \frac{\partial}{\partial z} C) / H_{bot}$

$H_{bot}$  Is the thickness of the box next to the bottom

$B_u=0.8$  – burial coefficient

**Mn(IV),Fe(III):**  $Q_{C_i} = 0$

**NH<sub>4</sub>, PO<sub>4</sub>:**  $Q_{C_i} = \tau_L^{-1} (C_{Li} - C_i)$

$\tau_L^{-1} = 6000$  s, is the relaxation time scale

$C_{NH4}=10 \mu M, C_{PO4}=4.5 \mu M$

**H<sub>2</sub>S,Mn(II), Fe(II) :**  $Q_{C_i} = F_{bf}(O_2) \tau_L^{-1} (C_{Li} - C_i)$

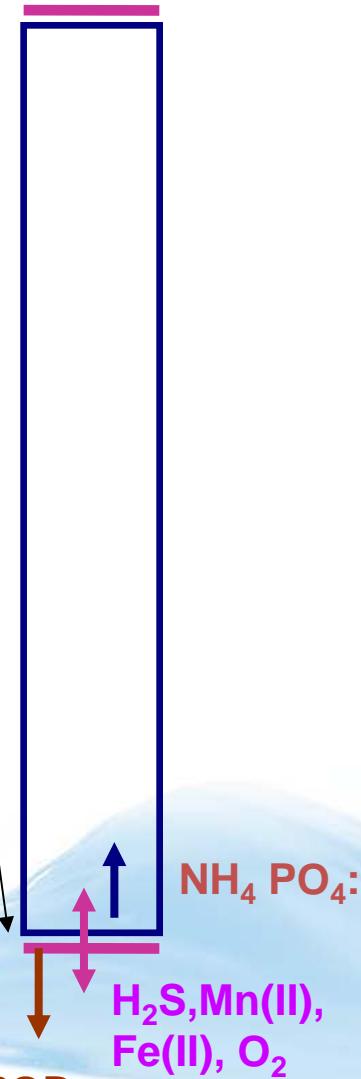
$F_{bf}(O_2) = (1 - 0.5(1 - \tanh(O_2^{bf} - O_2)))$  is the dependence on O<sub>2</sub>

$C_{H2S}=40 \mu M, C_{Mn(II)}=10 \mu M, C_{Fe(II)}=0.4 \mu M$

**O<sub>2</sub>:**  $Q_{C_i} = F_{bf}'(O_2) \tau_L^{-1} (C_{Li} - C_i)$

$F_{bf}'(O_2) = 0.5(1 - \tanh(O_2^{bf} - O_2))$  is the dependence on O<sub>2</sub>

$C_{O2}=0 \mu M$



# Stable balanced situation:

